

## P3 2 Thermal Insulation of Hobbit Holes Comfort in the Shire

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### Abstract

This paper analyses the thermal insulation of *Bag End* using precise scaling from Fonstad’s plan, yielding a total floor (and ceiling area) of  $182 \text{ m}^2$  with  $208 \text{ m}^2$  of lateral external wall area. With earth berm construction ( $R$ -value =  $12.59 \text{ m}^2\text{K}/\text{W}$ ) maintaining  $293 \text{ K}$  during the  $263 \text{ K}$  winters, steady-state heat loss is  $\sim 760 \text{ W}$  ( $4.2 \text{ W}/\text{m}^2$ ). The long hallway contributes significantly to heat loss but burial depth and material selection enable sustainable heating with  $\sim 18 \text{ kg}$  of wood daily.

### Introduction

The iconic *Hobbit-hole*, or “*smial*,” described in J.R.R. Tolkien’s work, presents a fascinating architectural puzzle [1]. Taking *Bag End* as our model, a spacious  $182 \text{ m}^2$  home buried  $3 \text{ m}$  deep in *Hobbiton Hill*, we ask a simple question: Could its earth and wood construction fend off a *Shire* winter, where temperatures can plunge to  $\sim 263 \text{ K}$  [2, 3]?

To find out, we model the structure using an average dry loamy soil ( $k_{\text{soil}} = 0.25 \text{ W}/\text{m}\cdot\text{K}$  [4]) and an upper bound oak wood lining ( $k_{\text{wood}} = 0.17 \text{ W}/\text{m}\cdot\text{K}$  [5]), targeting a  $\sim 293 \text{ K}$  inside. We calculate conductive heat loss under steady-state conditions, including both lateral walls and ceilings. This leads to insights on practical firewood needs for the *Baggins*’ during a cold night.

### Thermal Insulation Calculations

We start with the thermal resistance, or  $R$ -value, for each material:

$$R = \frac{d}{k}. \quad (1)$$

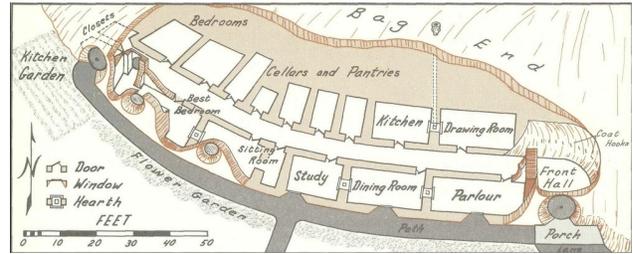


Figure 1: Fonstad’s Bag End floor plan with scale [3].

For the  $3 \text{ m}$  wall of soil ( $k_{\text{soil}} = 0.25 \text{ W}/\text{m}\cdot\text{K}$ ), this gives  $R_{\text{soil}} = 12 \text{ m}^2\text{K}/\text{W}$ . The interior wood lining, about  $0.1 \text{ m}$  thick ( $k_{\text{wood}} = 0.17 \text{ W}/\text{m}\cdot\text{K}$ ), adds  $R_{\text{wood}} \approx 0.59 \text{ m}^2\text{K}/\text{W}$ . Combined, the total resistance is  $R_{\text{total}} = 12.59 \text{ m}^2\text{K}/\text{W}$ . The overall heat transfer coefficient ( $U$ -value) is  $U = \frac{1}{12.59} \approx 0.079 \text{ W}/\text{m}^2\text{K}$ . To find the heat loss, we apply Fourier’s law:

$$Q = UA\Delta T. \quad (2)$$

The total area of the lateral external wall, derived from careful scaling of Fonstad’s plan [3], is

Room	Length (m)	Width (m)	Floor Area (m <sup>2</sup> )	External Wall Area (m <sup>2</sup> )	Q (W)
<b>Heated Rooms</b>					
Bedroom 1	3.6	3.3	11.9	12.4	29.0
Bedroom 2	3.6	3.3	11.9	12.4	29.0
Best Bedroom	7.3	3.3	24.1	19.1	45.0
Kitchen	4.5	3.0	13.5	13.5	32.0
Drawing Room	6.4	2.7	17.3	17.5	41.0
Dining Room	4.3	3.0	12.9	13.1	31.0
Study Parlour	7.6	2.7	20.5	19.4	46.0
Hallway	30.5	1.8	54.9	58.1	138.0
<b>Cold Storage</b>					
Cellar 1	1.8	4.3	7.7	11.2	0
Cellar 2	1.2	1.8	2.2	5.4	0
Cellar 3	1.8	3.0	5.4	8.6	0
Cellar 4	1.8	3.0	5.4	8.6	0
Cellar 5	1.8	3.0	5.4	8.6	0
<b>Total</b>			<b>182.1</b>	<b>207.5</b>	<b>391.0</b>

Table 1: Detailed room-by-room analysis of Bag End from precise scaling of Fonstad’s plan [3]. Cold storage pantries contribute zero to heat loss by design.

$\sim 208 \text{ m}^2$ . A detailed, room-by-room breakdown is provided in Table 1. To account for heat loss through the ceiling (assumed to have the same  $R$  value, with uniform 3 m soil coverage for simplification), we add the ceiling area, equal to the floor area per room. This yields a total surface area of  $\sim 208 \text{ m}^2$  (lateral) +  $182 \text{ m}^2$  (ceiling) =  $390 \text{ m}^2$ . We assume a temperature difference ( $\Delta T$ ) of 30 K between the  $\sim 293 \text{ K}$  interior and the harsh  $\sim 263 \text{ K}$  outside, excluding the unheated pantries where  $\Delta T = 0$  for both walls and ceilings (cold storage floor/ceiling =  $26 \text{ m}^2$ , lateral walls =  $42 \text{ m}^2$ ). The effective heated surface area is thus  $165 \text{ m}^2$  (heated lateral) +  $156 \text{ m}^2$  (heated ceiling) =  $321 \text{ m}^2$ . This yields a total heat loss rate,  $Q_{\text{total}}$ , of about 760 W. We neglect heat loss through the floor, assuming the deep earth remains at a stable temperature.

## Discussion

Our calculated heat loss of 760 W ( $4.2 \text{ W/m}^2$ ) under steady-state reveals a dwelling of great efficiency, surpassing modern passive house standards ( $< 10 \text{ W/m}^2$  [6]). The generous  $182 \text{ m}^2$  floor area fits the original works, confirming *Bag End’s* reputation as the “most luxurious” *smial* in *Hobbiton* [1].

A key finding is the role of the hallway, which

alone accounts for 35% of the lateral wall heat loss (138 W).

The four fireplaces (each  $\sim 1.25 \text{ kW}$  at 20% efficiency [7]) provide  $\sim 1000 \text{ W}$  effective input. Meeting the daily energy need ( $18.2 \text{ kWh}$  or  $65.7 \text{ MJ}$ ) requires  $\sim 18 \text{ kg}$  of dry oak wood ( $18 \text{ MJ/kg}$  [8] usable at  $3.6 \text{ MJ/kg}$  efficiency). Entropy generation,

$$\Delta S = \frac{Q}{T_{\text{out}}} - \frac{Q}{T_{\text{in}}} \quad (3)$$

( $T_{\text{in}} = 293 \text{ K}$ ,  $T_{\text{out}} = 263 \text{ K}$ ), is  $\sim 0.30 \text{ J/K}\cdot\text{s}$  — far lower than for an above-ground equivalent ( $0.60 \text{ J/K}\cdot\text{s}$  at  $Q = 1724 \text{ W}$ ), highlighting the thermodynamic advantage.

## Conclusion

*Bag End’s* earth-sheltered design exemplifies efficient thermal insulation, with ceiling inclusion and low hygrothermal risks enabling minimal heating in harsh winters. This analysis bridges Tolkien’s fantasy with real physics, showing how burial depth, material choices, and climate interplay for sustainable comfort. Future work could incorporate, and take into account, the geothermal phenomenon of the thermal mass of the Earth itself, which would act as a seasonal heat reservoir for greater accuracy — on a *Hobbit’s* scale.

## References

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